

# SIP panel

## Thermal protection

$U = 0,13 \text{ W/(m}^2\text{K)}$

GEG 2020/24 Bestand\*:  $U < 0,24 \text{ W/(m}^2\text{K)}$



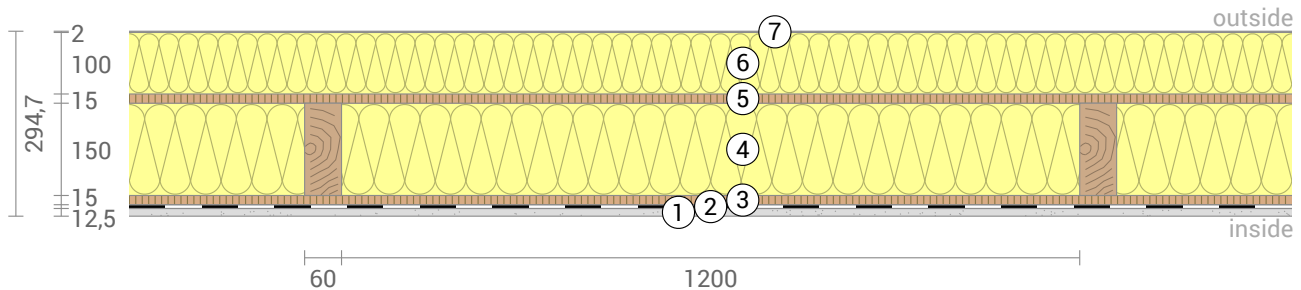
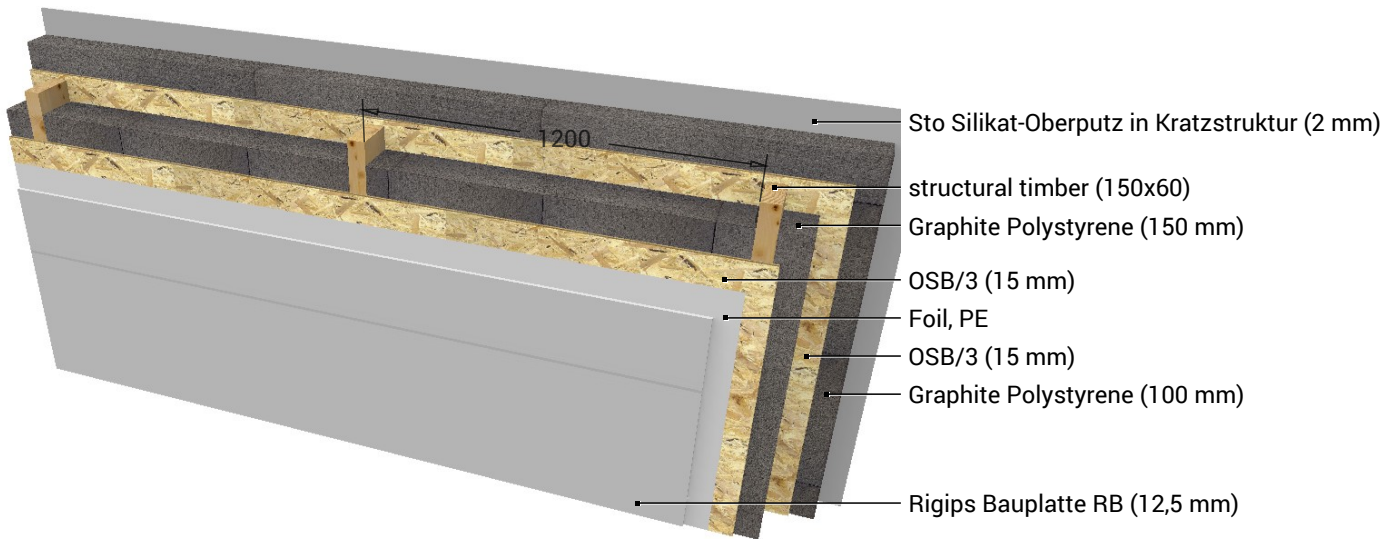
## Moisture proofing

Drying reserve:  $178 \text{ g/m}^2\text{a}$   
No condensate



## Heat protection

Temperature amplitude damping: 38  
phase shift: 11,2 h  
Thermal capacity inside:  $36 \text{ kJ/m}^2\text{K}$



- ① Rigips Bauplatte RB (12,5 mm)
- ② Foil, PE
- ③ OSB/3 (15 mm)
- ④ Graphite Polystyrene (150 mm)
- ⑤ OSB/3 (15 mm)
- ⑥ Graphite Polystyrene (100 mm)
- ⑦ Sto Silikat-Oberputz in Kratzstruktur (2 mm)

Inside air :  $20,0^\circ\text{C} / 50\%$   
Outside air:  $-5,0^\circ\text{C} / 80\%$   
Surface temperature.:  $18,7^\circ\text{C} / -4,9^\circ\text{C}$

sd-value:  $35,1 \text{ m}$   
Drying reserve:  $178 \text{ g/m}^2\text{a}$

Thickness:  $29,5 \text{ cm}$   
Weight:  $38 \text{ kg/m}^2$   
Heat capacity:  $54 \text{ kJ/m}^2\text{K}$

- GEG 2020/24 Bestand
- BEG Einzelmaßn.
- GEG 2023/24 Neubau
- DIN 4108

\*Comparison of the U-value with den Höchstwerten aus GEG Anlage 7 (GEG 2020-2024 Bestand); den techn. Mindestanforderungen für BEG Einzelmaßnahmen; 70% des U-Werts der Referenzausführung aus GEG 2023/2024 Anlage 1 (GEG Neubau); den R-Werten aus DIN 4108-2 Tabelle 3

SIP panel,  $U=0,13 \text{ W}/(\text{m}^2\text{K})$

## U-Value calculation according to DIN EN ISO 6946

#	Material	Dicke [cm]	$\lambda$ [W/mK]	R [m <sup>2</sup> K/W]
	Thermal contact resistance inside (Rsi)			0,130
1	Rigips Bauplatte RB	1,25	0,250	0,050
2	Foil, PE	0,02	0,400	0,001
3	OSB/3	1,50	0,130	0,115
4	Graphite Polystyrene (GPS)	15,00	0,032	4,688
	structural timber (4,8%)	15,00	0,130	1,154
5	OSB/3	1,50	0,130	0,115
6	Graphite Polystyrene (GPS)	10,00	0,032	3,125
7	Sto Silikat-Oberputz in Kratzstruktur	0,20	0,700	0,003
	Thermal contact resistance outside (Rse)			0,040

Thermal contact resistances have been taken from DIN 6946 Table 7.

Rsi: heat flow direction horizontally

Rse: heat flow direction horizontally, outside: Direct contact to outside air

Upper limit of thermal resistance  $R_{\text{tot;upper}} = 7,983 \text{ m}^2\text{K}/\text{W}$ .

Lower limit of thermal resistance  $R_{\text{tot;lower}} = 7,670 \text{ m}^2\text{K}/\text{W}$ .

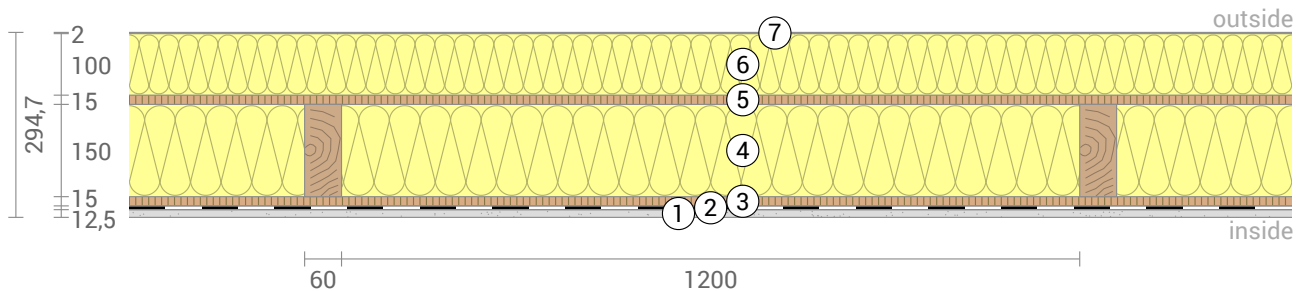
Check applicability:  $R_{\text{tot;upper}} / R_{\text{tot;lower}} = 1,041$  (maximum allowed: 1,5)

The procedure may be used.

Thermal resistance  $R_{\text{tot}} = (R_{\text{tot;upper}} + R_{\text{tot;lower}})/2 = 7,826 \text{ m}^2\text{K}/\text{W}$

Estimated maximum relative uncertainty according to section 6.7.2.5: 2,0%

Heat transfer coefficient  $U = 1/R_{\text{tot}} = 0,13 \text{ W}/(\text{m}^2\text{K})$



SIP panel, U=0,13 W/(m<sup>2</sup>K)

LCA

Heat loss: 10 kWh/m<sup>2</sup> per heating season



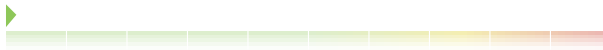
Amount of heat that escapes through one square meter of this component during the heating period. Please note: Due to internal and solar gains, the heating demand is lower than the heat loss.

Primary energy (non renewable): 191 kWh/m<sup>2</sup>



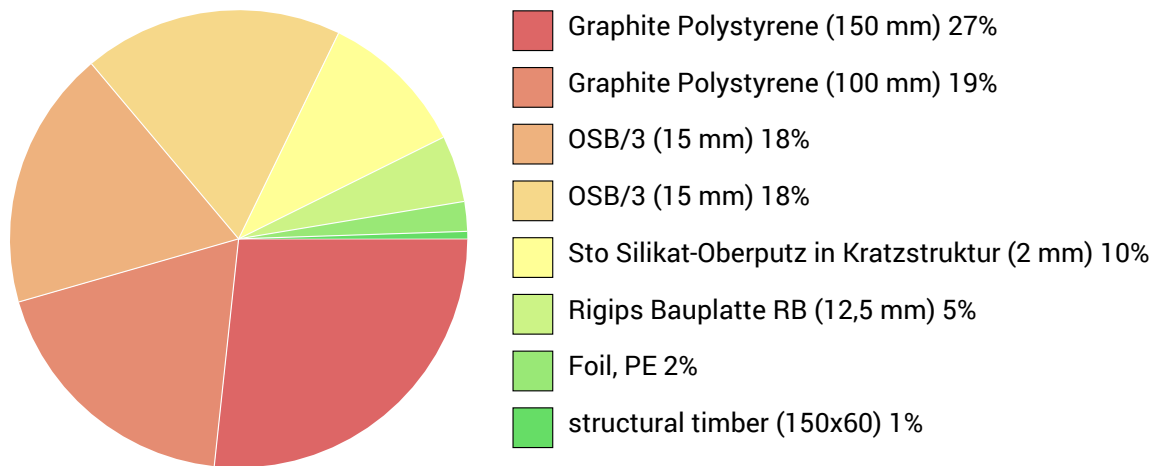
Non-renewable primary energy (= energy from fossil fuels and nuclear energy) that was used to produce the new building materials ("cradle to gate").

Green house gas potential: -5,4 kg CO<sub>2</sub> Äqv./m<sup>2</sup>

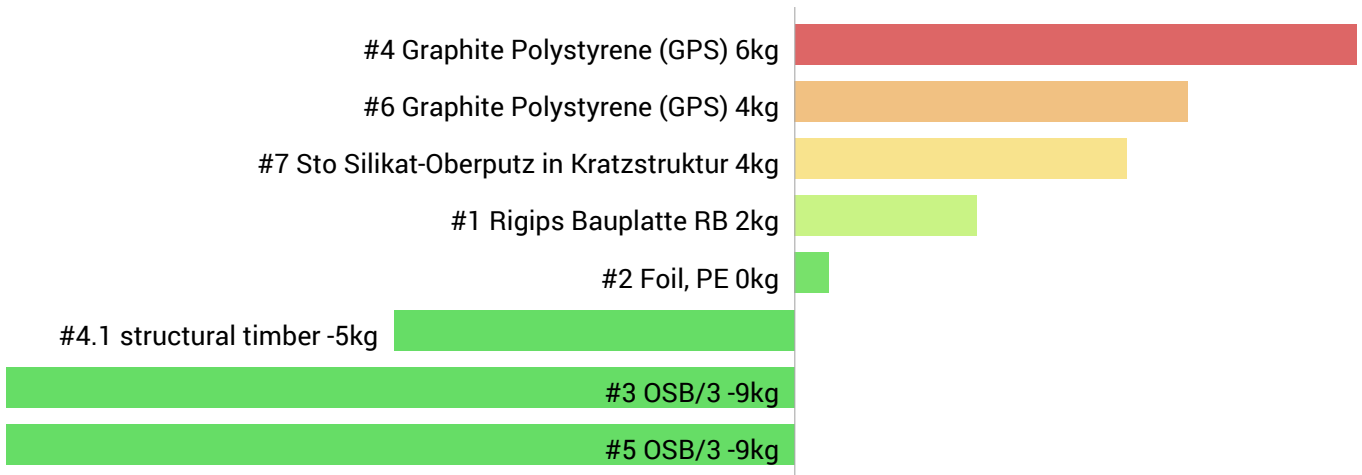


For the production of the building materials used, more greenhouse gases were withdrawn from the atmosphere than emitted.

Composition of non-renewable primary energy of production:

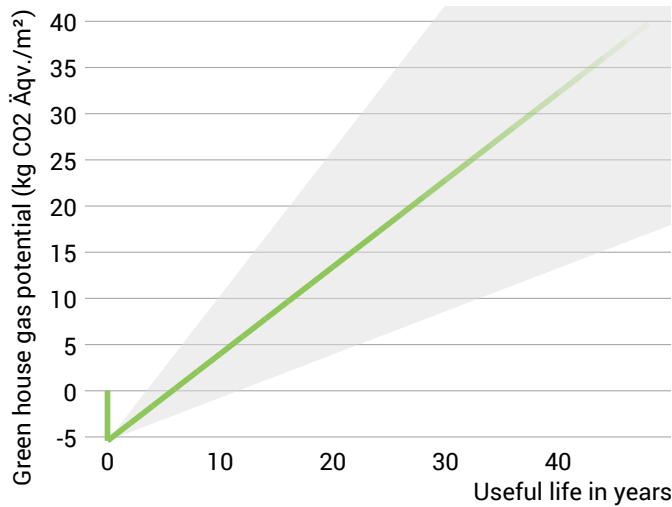


Composition of the greenhouse potential of production:



SIP panel,  $U=0,13 \text{ W}/(\text{m}^2\text{K})$

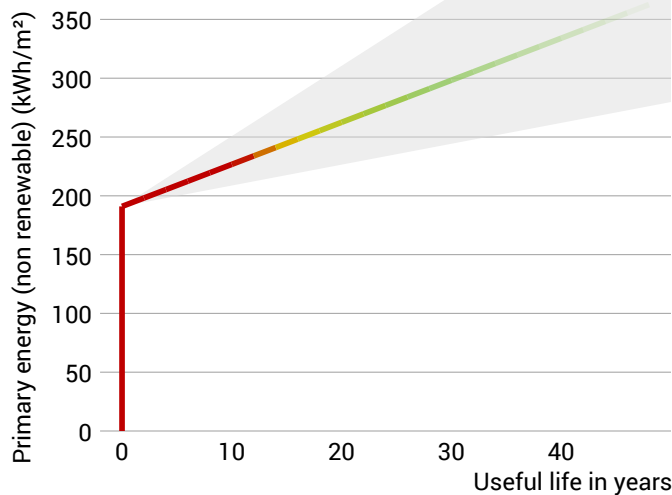
## Global warming potential and primary energy for construction and use



The **left figure** shows the global warming potential of the production of the component in the vertical part of the curve. Greenhouse gas emissions (through heating) arising during use of the building are indicated by the upward curve.

The **figure at the bottom left** shows the non-renewable primary energy expenditure for the production of the component in the vertical part of the curve. The primary energy required during use of the building (through heating) is represented by the upward curve.

The longer the component is used unchanged, the more environmentally friendly it is, because the production costs contribute less to the total emissions (indicated by the color of the curve).



Due to unknown solar and internal gains, the heating demand can only be estimated. Accordingly, primary energy consumption and global warming potential during the use phase are only vaguely known. For the estimation it was assumed that solar and internal profits contribute with  $4 \text{ kWh}/\text{a}/\text{m}^2$  component area. The light gray area indicates the area in which the curve is located with great certainty. For heat generation, a primary energy input of  $0,60 \text{ kWh}$  per  $\text{kWh}$  of heat and a global warming potential of  $0,16 \text{ kg CO}_2 \text{ eqv}/\text{m}^2$  per  $\text{kWh}$  of heat was used. Heat source: Heat pump (air-water).

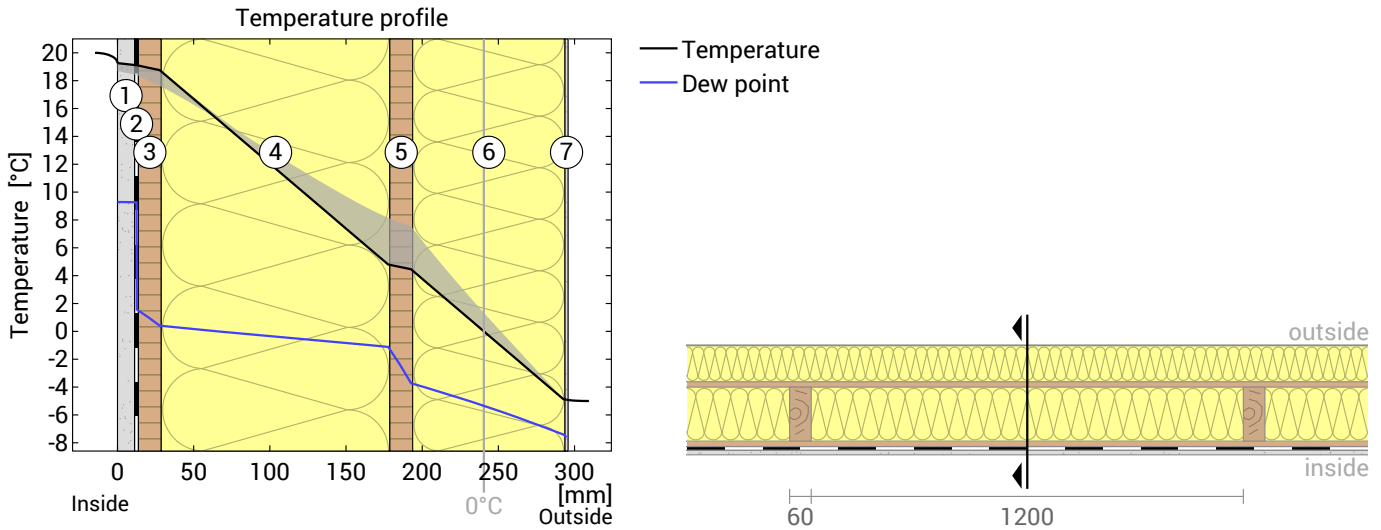
### Hints

Calculated for the location DIN V 18599, heating period from Mid of October to End of April. The calculation is based on monthly average temperatures. Source: DIN V 18599-10:2007-02

The climate and energy data on which this calculation is based can, in some cases, show considerable fluctuations and, in individual cases, deviate considerably from the actual value.

SIP panel,  $U=0,13 \text{ W}/(\text{m}^2\text{K})$

## Temperature profile



- ① Rigips Bauplatte RB (12,5 mm)
- ② Foil, PE
- ③ OSB/3 (15 mm)
- ④ Graphite Polystyrene (150 mm)
- ⑤ OSB/3 (15 mm)
- ⑥ Graphite Polystyrene (100 mm)
- ⑦ Sto Silikat-Oberputz in Kratzstrukt...

**Left:** Temperature and dew-point temperature at the place marked in the right figure. The dew-point indicates the temperature, at which water vapour condensates. As long as the temperature of the component is everywhere above the dew point, no condensation occurs. If the curves have contact, condensation occurs at the corresponding position.

**Right:** The component, drawn to scale.

## Layers (from inside to outside)

#	Material	$\lambda$ [W/mK]	R [m <sup>2</sup> K/W]	Temperatur [°C]		Weight [kg/m <sup>2</sup> ]
				min	max	
	Thermal contact resistance*		0,250	18,7	20,0	
1	1,25 cm Rigips Bauplatte RB	0,250	0,050	18,4	19,3	8,5
2	0,02 cm Foil, PE	0,400	0,001	18,4	19,1	0,2
3	1,5 cm OSB/3	0,130	0,115	17,6	19,1	9,3
4	15 cm Graphite Polystyrene (GPS)	0,032	4,688	4,8	18,8	2,1
	15 cm structural timber (4,8%)	0,130	1,154	8,1	17,9	3,0
5	1,5 cm OSB/3	0,130	0,115	4,5	8,1	9,3
6	10 cm Graphite Polystyrene (GPS)	0,032	3,125	-4,9	7,5	1,5
7	0,2 cm Sto Silikat-Oberputz in Kratzstruktur	0,700	0,003	-4,9	-4,8	4,0
	Thermal contact resistance*		0,040	-5,0	-4,9	
29,47 cm Whole component			7,814			37,9

\*Thermal contact resistances according to DIN 4108-3 for moisture protection and temperature profile. The values for the U-value calculation can be found on the page 'U-value calculation'.

Surface temperature inside (min / average / max): 18,7°C 19,2°C 19,3°C  
 Surface temperature outside (min / average / max): -4,9°C -4,9°C -4,9°C

SIP panel,  $U=0,13 \text{ W}/(\text{m}^2\text{K})$

## Moisture proofing

For the calculation of the amount of condensation water, the component was exposed to the following constant climate for 90 days: inside: 20°C und 50% Humidity; outside: -5°C und 80% Humidity. This climate complies with DIN 4108-3.

This component is free of condensate under the given climate conditions.

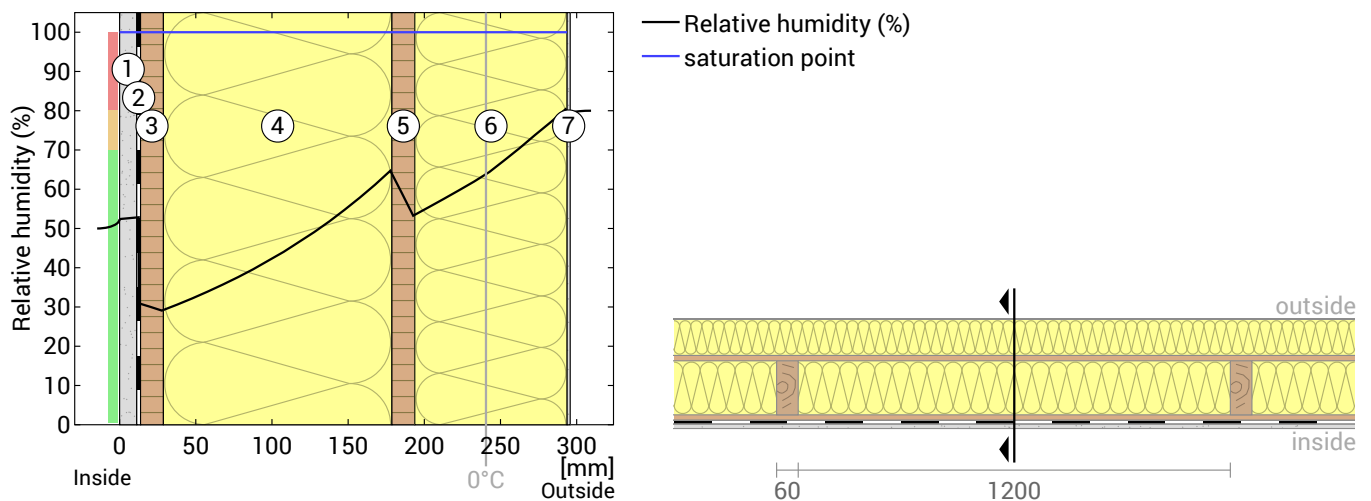
Drying reserve according to DIN 4108-3:2024: 178 g/(m<sup>2</sup>a)  
At least required by DIN 68800-2: 100 g/(m<sup>2</sup>a)

#	Material	sd-value [m]	Condensate [kg/m <sup>2</sup> ] [Gew.-%]	Weight [kg/m <sup>2</sup> ]
1	1,25 cm Rigips Bauplatte RB	0,05	-	8,5
2	0,02 cm Foil, PE	20,00	-	0,2
3	1,5 cm OSB/3	2,25	-	9,3
4	15 cm Graphite Polystyrene (GPS)	3,00	-	2,1
	15 cm structural timber (4,8%)	6,00	-	3,0
5	1,5 cm OSB/3	4,50	-	9,3
6	10 cm Graphite Polystyrene (GPS)	5,00	-	1,5
7	0,2 cm Sto Silikat-Oberputz in Kratzstruktur	0,22	-	4,0
	29,47 cm Whole component	35,14	0	37,9

## Humidity

The temperature of the inside surface is 18,7 °C leading to a relative humidity on the surface of 54%. Mould formation is not expected under these conditions.

The following figure shows the relative humidity inside the component.



- ① Rigips Bauplatte RB (12,5 mm)
- ② Foil, PE
- ③ OSB/3 (15 mm)
- ④ Graphite Polystyrene (150 mm)
- ⑤ OSB/3 (15 mm)
- ⑥ Graphite Polystyrene (100 mm)
- ⑦ Sto Silikat-Oberputz in Kratzstrukt...

Notes: Calculation using the Ubakus 2D-FE method. Convection and the capillarity of the building materials were not considered. The drying time may take longer under unfavorable conditions (shading, damp / cool summers) than calculated here.

SIP panel,  $U=0,13 \text{ W}/(\text{m}^2\text{K})$

## Moisture protection in accordance with DIN 4108-3:2024 Appendix A

Dieser Feuchteschutznachweis ist nur bei **nicht klimatisierten** Wohn- oder wohnähnlich genutzten Gebäuden gültig, die auf einer Höhe von max. 700m NN liegen.

Please note the hints at the end of these moisture proofing calculations.

#	Material	$\lambda$ [W/mK]	R [m <sup>2</sup> K/W]	sd [m]	$\rho$ [kg/m <sup>3</sup> ]	T [°C]	ps [Pa]	$\Sigma$ sd [m]
Thermal contact resistance			0,250					
1	1,25 cm Rigips Bauplatte RB	0,250	0,050	0,05	680	19,25	2232	0
2	0,02 cm Foil, PE	0,400	0,001	20	930	19,11	2211	0,05
3	1,5 cm OSB/3	0,130	0,115	2,25	620	19,10	2211	20,1
4	15 cm Graphite Polystyrene (GPS)	0,032	4,688	3	15	18,76	2164	22,3
5	1,5 cm OSB/3	0,130	0,115	4,5	620	4,79	859	25,3
6	10 cm Graphite Polystyrene (GPS)	0,032	3,125	5	15	4,44	839	29,8
7	0,2 cm Sto Silikat-Oberputz in Kratzstruktur	0,700	0,003	0,22	2000	-4,87	406	34,8
Thermal contact resistance			0,040			-4,88	405	35

Temperature (T), vapor saturation pressure (ps), and the sum of the sd-values ( $\Sigma$ sd) apply to the layer boundary.

### Relative air humidity on the surface

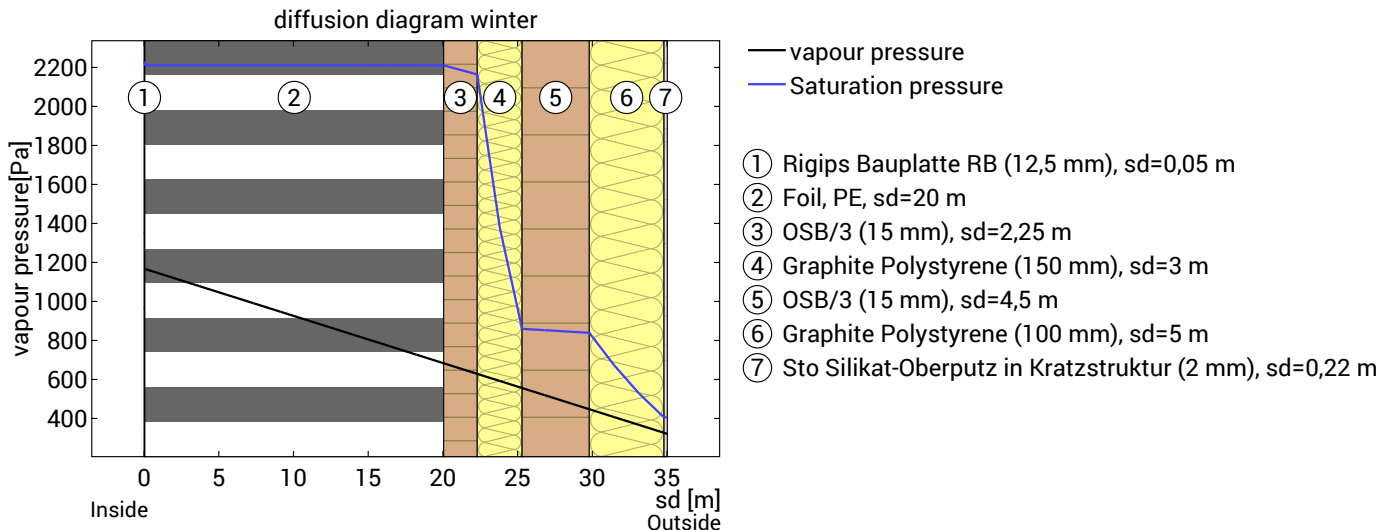
The relative humidity on the interior surface is 52%. Requirements for the prevention of building material corrosion depend on material and coating and have not been investigated.



### Dew period (winter)

#### Boundary conditions

Vapor pressure inside at 20°C and 50% humidity	$p_i = 1168 \text{ Pa}$
Vapor pressure outside at -5°C and 80% humidity	$p_e = 321 \text{ Pa}$
Duration of condensation period (90 days)	$t_c = 7776000 \text{ s}$
Water vapor diffusion coefficient in static air	$\delta_0 = 2.0E-10 \text{ kg}/(\text{m}^2\text{sPa})$
sd-value (Whole component.)	$s_{de} = 35,02 \text{ m}$



The section under investigation is free of condensate under the given climate conditions.



Calculate evaporation potential for the drying reserve in the dew period for the plane with the lowest evaporation potential:

$s_d=25,30 \text{ m}$ ;  $x=17,77 \text{ cm}$ ;  $p_s=859 \text{ pa}$ :

Layer boundary between Graphite Polystyrene (GPS) and OSB/3

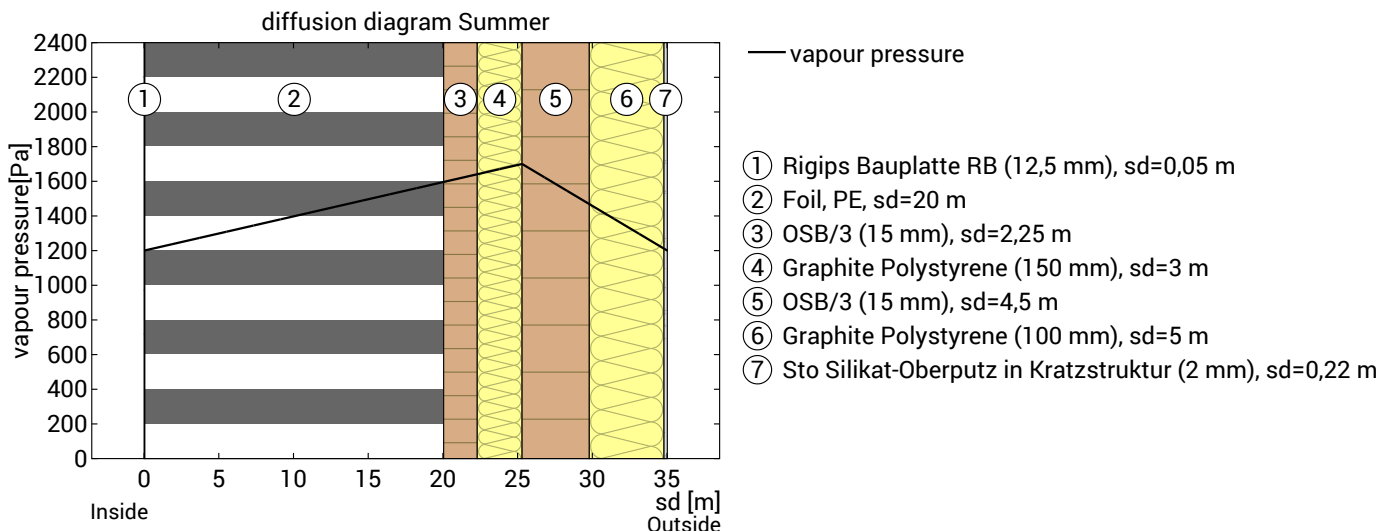
$$M_{ev, \text{Tauperiode}} = t_c \cdot \delta_0 \cdot ((p_s - p_i) / s_{d_{ev}} + (p_s - p_e) / (s_{d_e} - s_{d_{ev}})) = 0,067 \text{ kg}/\text{m}^2$$

SIP panel,  $U=0,13 \text{ W}/(\text{m}^2\text{K})$

### Evaporation period (summer)

#### Boundary conditions

Interior vapor pressure	$p_i = 1200 \text{ Pa}$
Exterior vapor pressure	$p_e = 1200 \text{ Pa}$
Saturation vapour pressure in the condensation area	$p_s = 1700 \text{ Pa}$
Length of drying season (90 days)	$t_{ev} = 7776000 \text{ s}$
sd-values remain unchanged.	



Condensate-free component: The maximum possible evaporation mass for the drying reserve is calculated. Consider the level that has the lowest evaporation potential in the dew period, at  $s_d=25,30 \text{ m}$ ;  $x=17,77 \text{ cm}$ :

Layer boundary between Graphite Polystyrene (GPS) and OSB/3

Evaporation mass:  $M_{ev} = \delta_0 \cdot t_{ev} \cdot [(p_s - p_i)/s_d + (p_s - p_e)/(s_{de} - s_d)] = 0,11 \text{ kg/m}^2$

#### Drying reserve (DIN 68800-2)

Dew-water-free component: The evaporation potential of the dew period is also taken into account.

Drying reserve:  $M_r = (M_{ev} + M_{ev, Tauperiode}) \cdot 1000 = 178 \text{ g/m}^2/\text{a}$

Minimum requested for walls and ceilings:  $100 \text{ g/m}^2/\text{a}$



#### Evaluation according to DIN 4108-3

The component is permissible regarding the moisture protection.

#### Hints

In the case of inhomogeneous constructions, such as skeleton-, stand- or frame constructions, as well as in wooden beam, rafter or half-timbered constructions or the like, the one-dimensional diffusion calculations are only to be demonstrated for the compartment area. Exceptional cases are special constructions in which, for example, The diffusion-inhibiting layer is also laid section-wise over the outer area. In these exceptional cases, the calculation performed here is invalid.

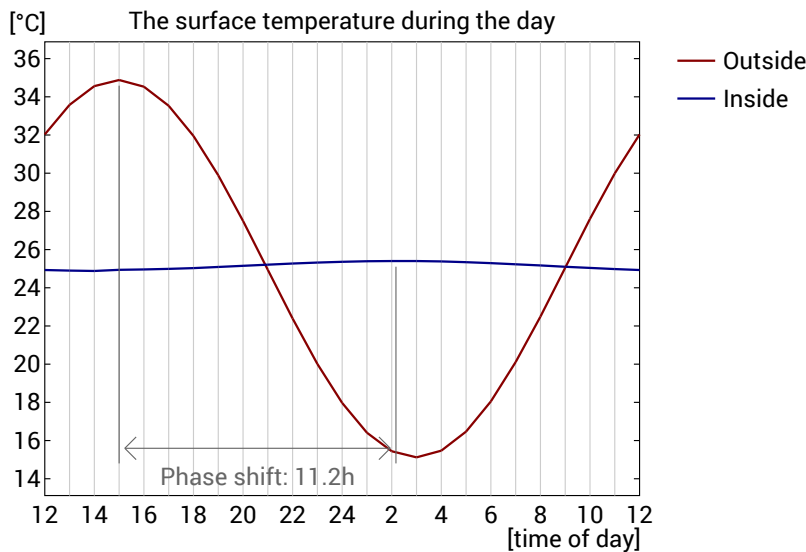
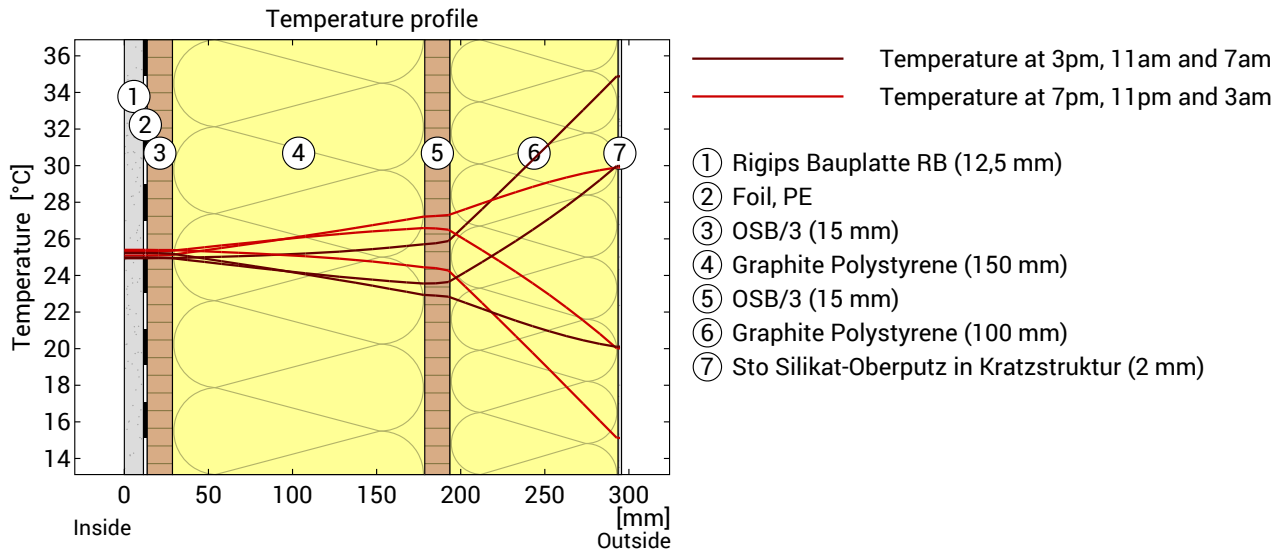
DIN 4108-3 describes in Section 5.3 components for which no moisture proofing is required as there is no risk of condensation water or the method is not suitable for the assessment. It is not possible to assess whether the component under test is underneath.



SIP panel, U=0,13 W/(m²K)

## Heat protection

The following results are properties of the tested component alone and do not make any statement about the heat protection of the entire room:



**Top:** Temperature profile within the component at different times. From top to bottom, brown lines: at 3 pm, 11 am and 7 am and red lines at 7 pm, 11 pm and 3 am.

**Bottom:** Temperature on the outer ( red ) and inner ( blue ) surface in the course of a day. The arrows indicate the location of the temperature maximum values. The maximum of the inner surface temperature should preferably occur during the second half of the night.

Phase shift*	11,2 h	Heat storage capacity (whole component):	54 kJ/m²K
Amplitude attenuation **	38,0	Thermal capacity of inner layers:	36 kJ/m²K
TAV ***	0,026		

\* The phase shift is the time in hours after which the temperature peak of the afternoon reaches the component interior.

\*\* The amplitude attenuation describes the attenuation of the temperature wave when passing through the component. A value of 10 means that the temperature on the outside varies 10x stronger than on the inside, e.g. outside 15-35 °C, inside 24-26 °C.

\*\*\* The temperature amplitude ratio TAV is the reciprocal of the attenuation: TAV = 1 / amplitude attenuation

Note: The heat protection of a room is influenced by several factors, but essentially by the direct solar radiation through windows and the total amount of heat storage capacity (including floor, interior walls and furniture). A single component usually has only a very small influence on the heat protection of the room.

The calculations presented above have been created for a 1-dimensional cross-section of the component.